



SPACE TRIPS SUMMER SCHOOL



Theme 9: SPACE

Riga Latvia

June 17-20 , 2 0 1 4

Thermoacoustic Electric Generation

P. Lotton, G. Poignand, G. Penelet, C. Olivier

Laboratoire d'Acoustique de l'Université du Maine

LAUM UMR 6613

Avenue Olivier Messiaen, 72085 Le Mans Cedex 09, France



Le Mans City

2



Laboratoire d'Acoustique de l'Université du Maine

3



UMR CNRS 6613



LAUM



Université
du Maine

Introduction

4

Patented Apr. 17, 1951

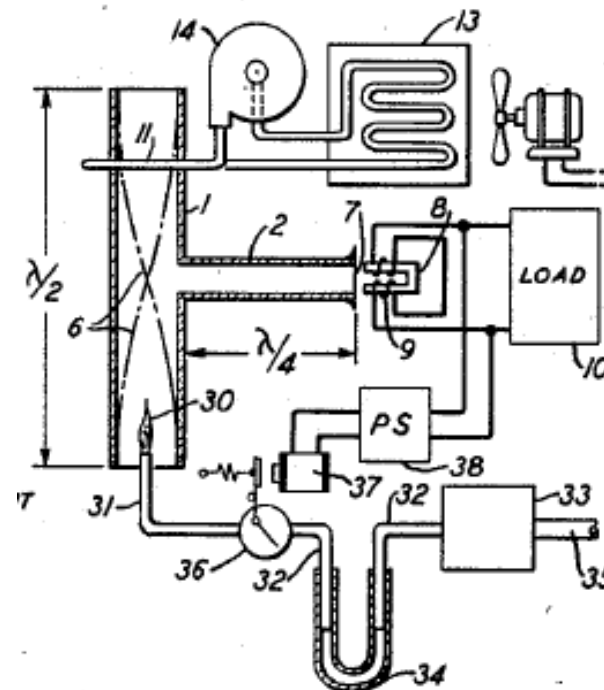
UNITED STATES PATENT OFFICE

2,549,464

ELECTRIC POWER SOURCE

Ralph V. L. Hartley, Summit, N. J., assignor to Bell Telephone Laboratories, Incorporated, New York, N. Y., a corporation of New York

FIG. 4



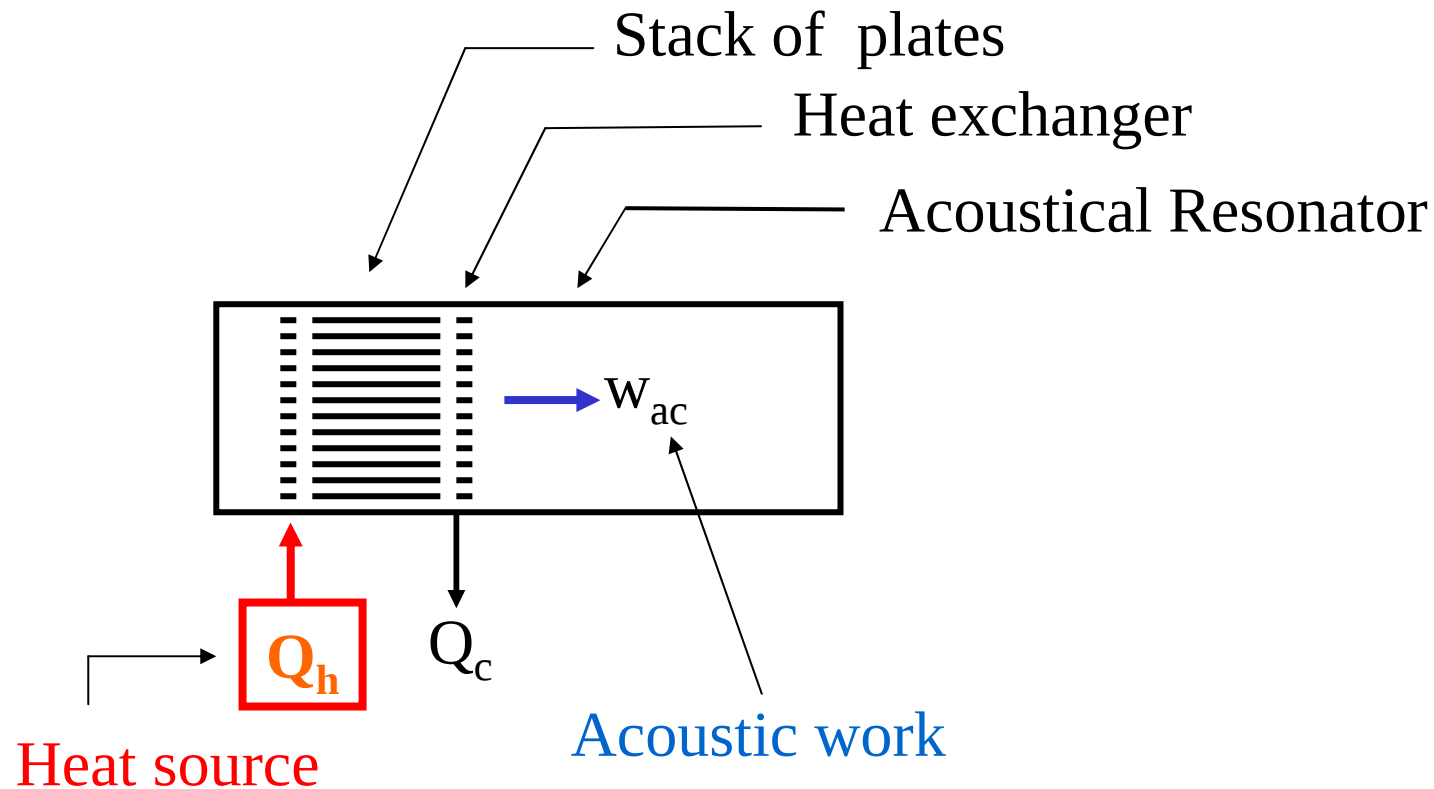
Outlines

5

- Introduction
- Theory
- Some realizations
- Future development

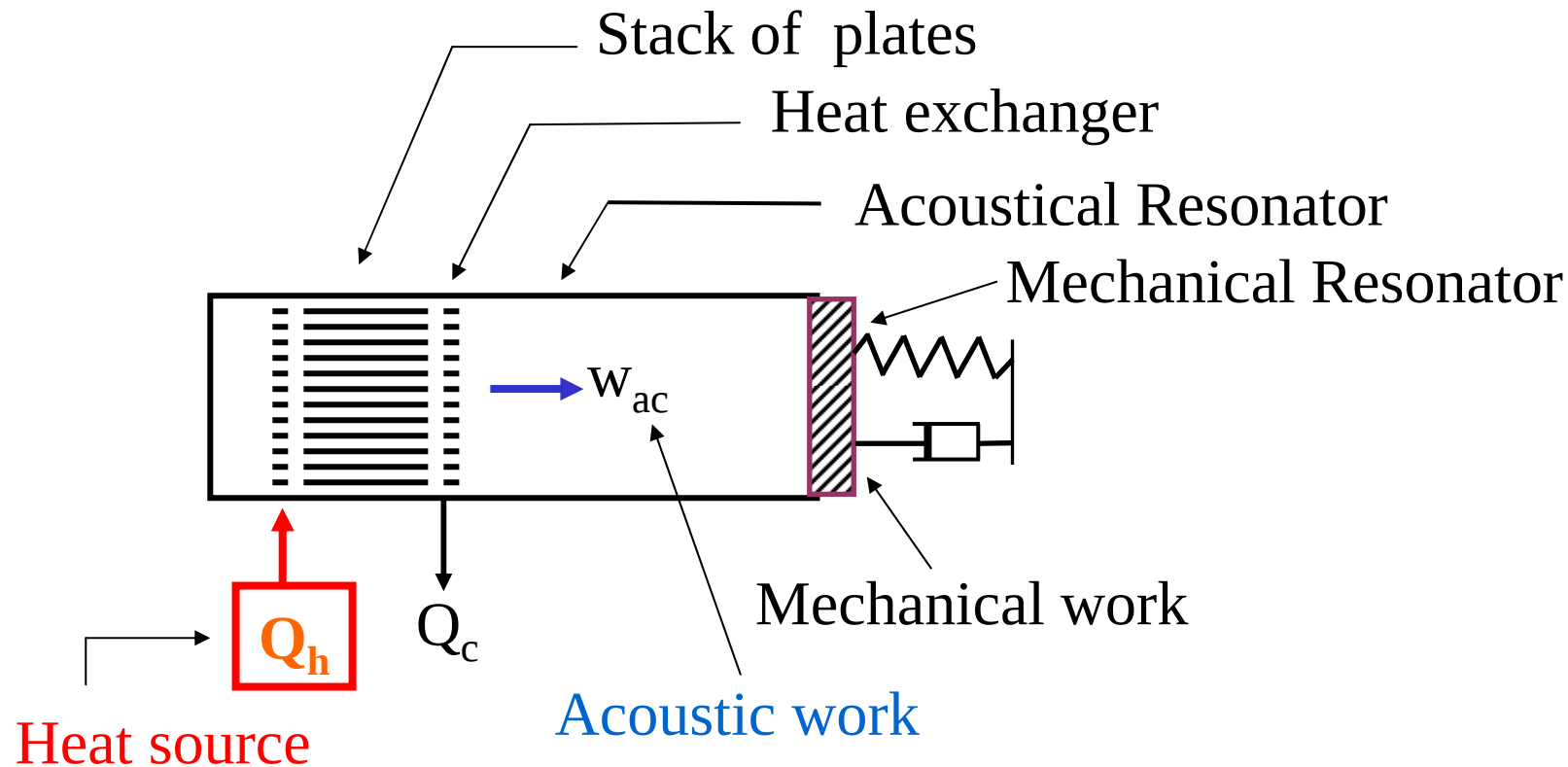
Thermoacoustic Engine

6



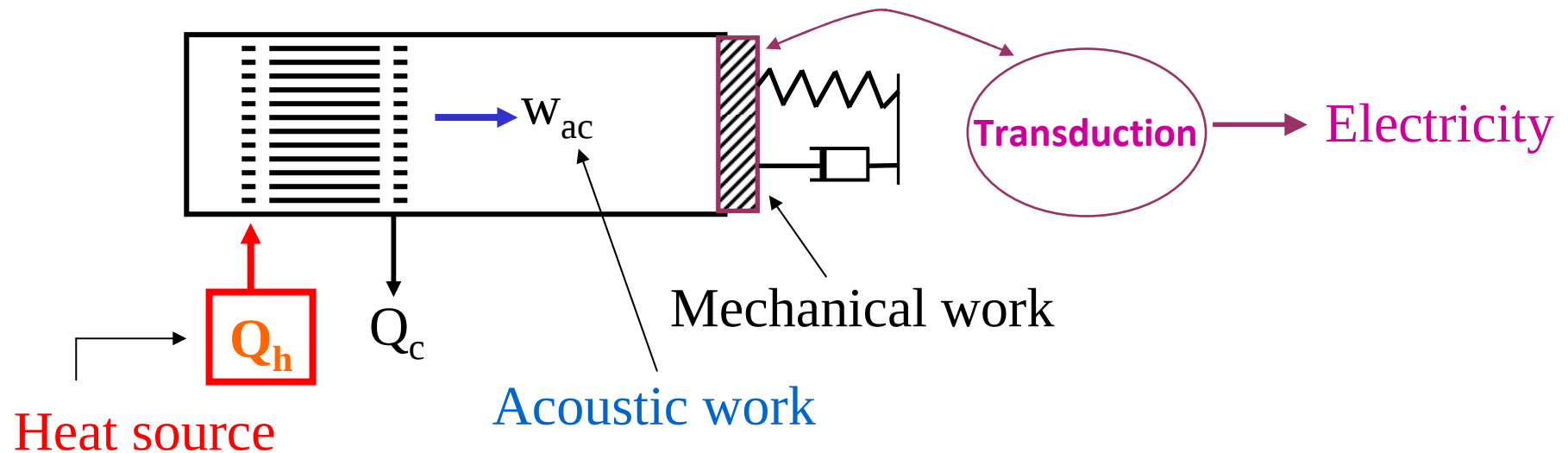
Thermo-acousto-mechanical^{Introduction} device

7



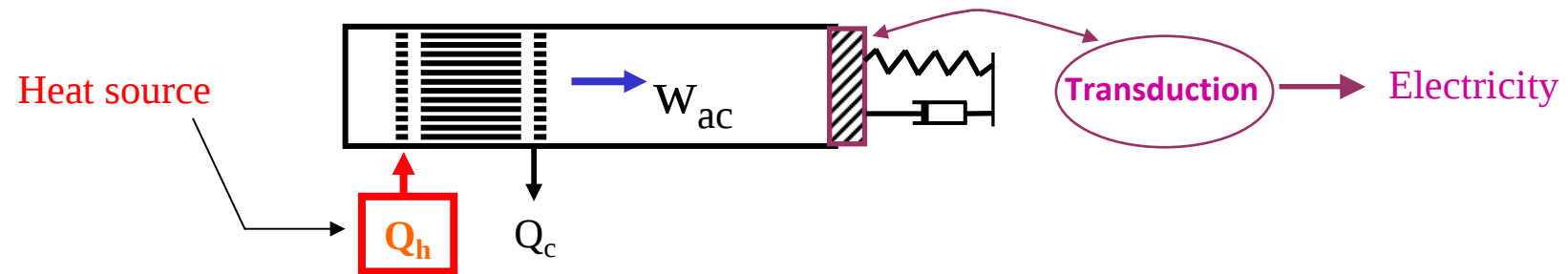
Thermo-acousto-mechanico-electrical^{Introduction} device

8



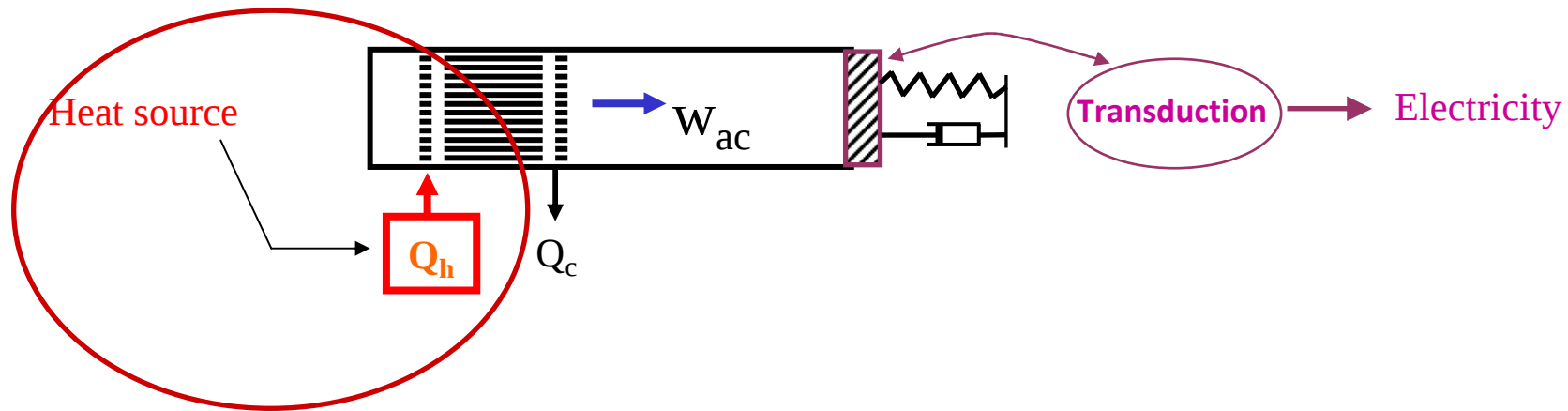
Different architectures

9



Different architectures

10

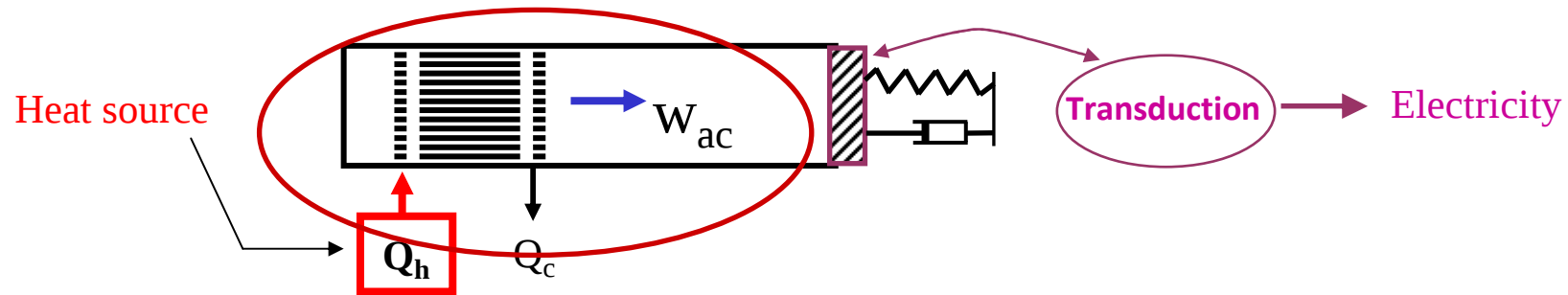


□ Heat source

- Solar dish
- Waste heat
- Biomass
-

Different architectures

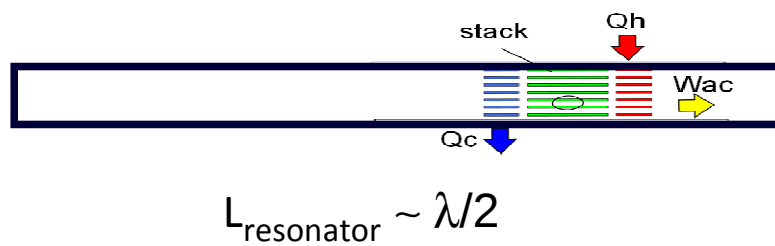
11



Resonator

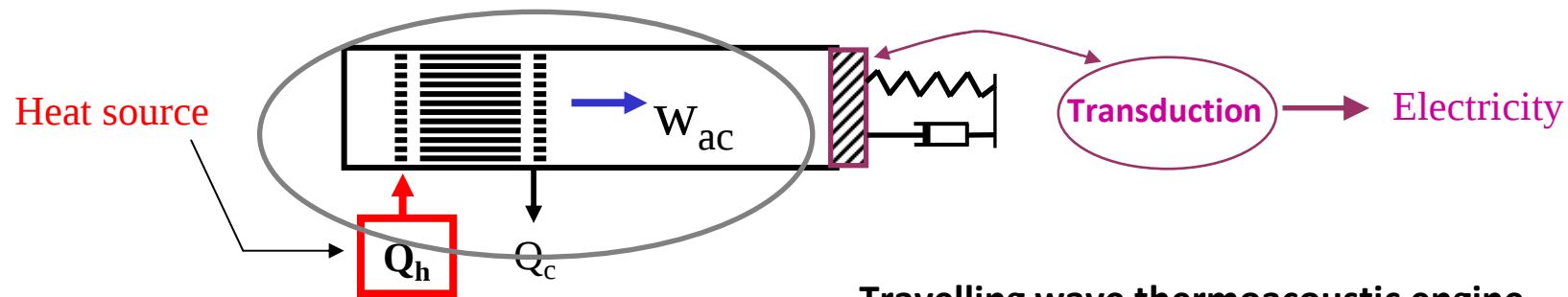
Standing wave thermoacoustic engine

- ▶ p and v are out of phase + stack



Different architectures

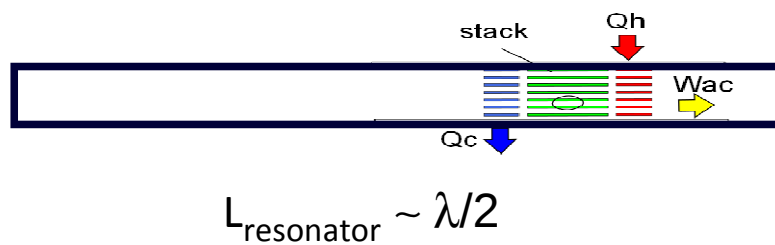
12



Resonator

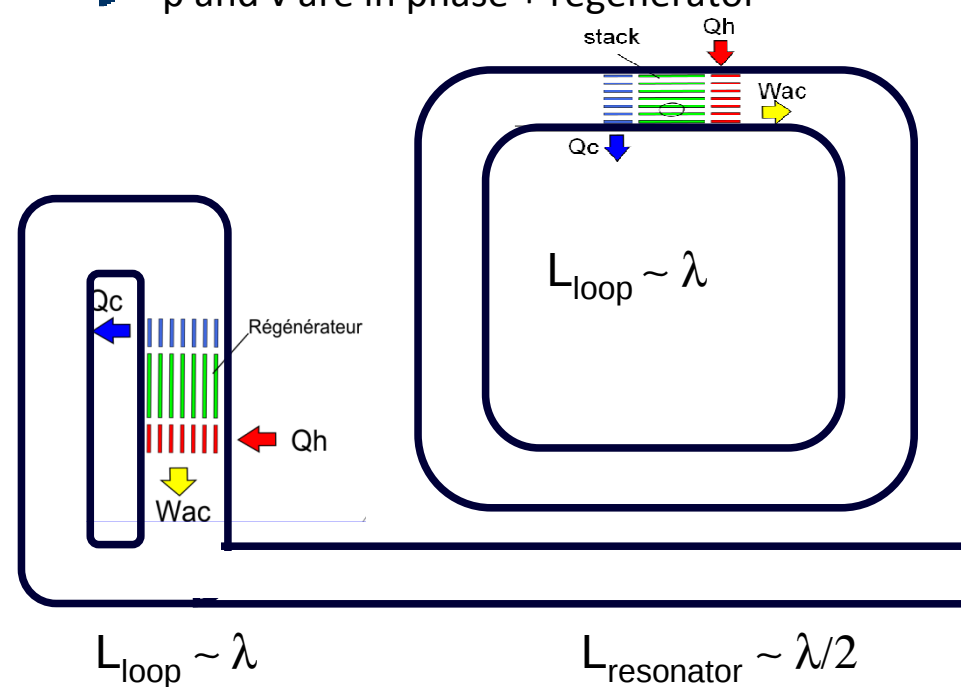
Standing wave thermoacoustic engine

- ▶ p and v are out of phase + stack



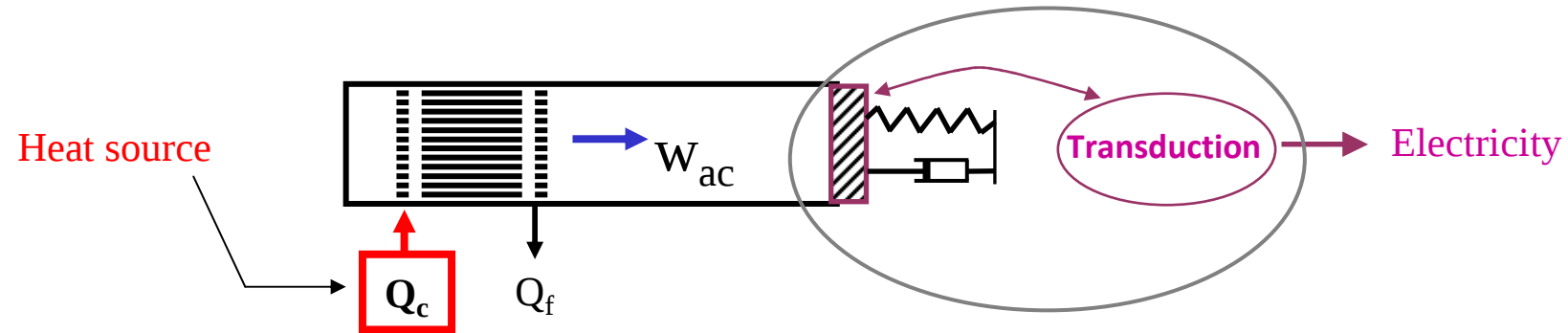
Travelling wave thermoacoustic engine

- ▶ p and v are in phase + regenerator



Different architectures

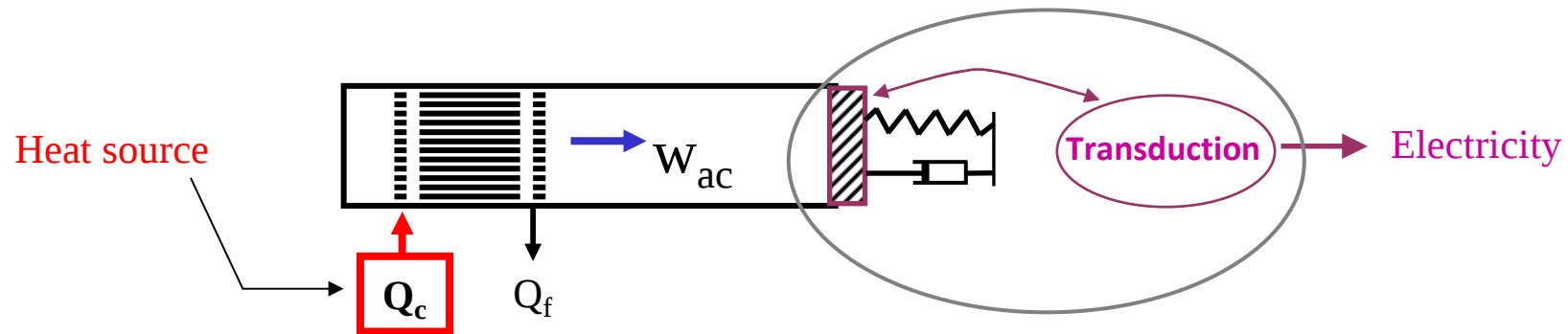
13



Electro-mechanical transducer

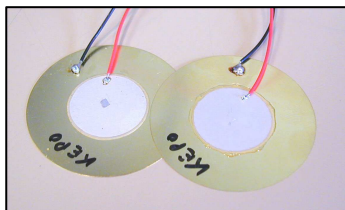
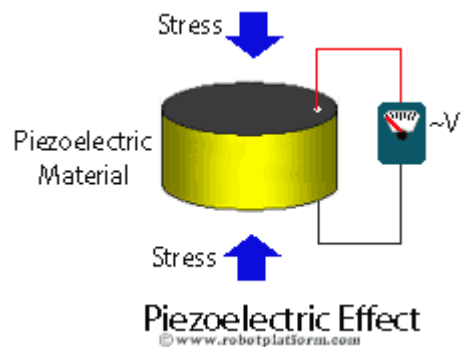
Different architectures

14



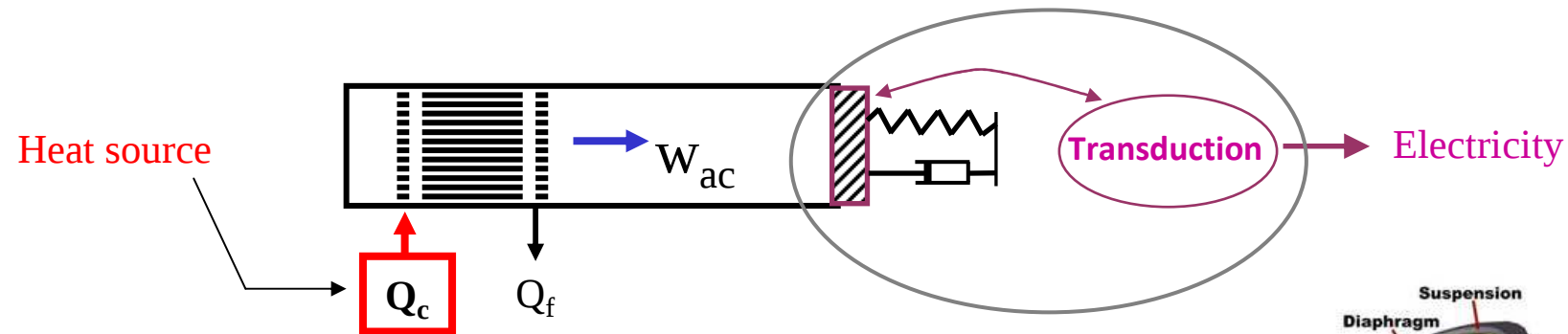
Electro-mechanical transducer

Piezoelectric sensors



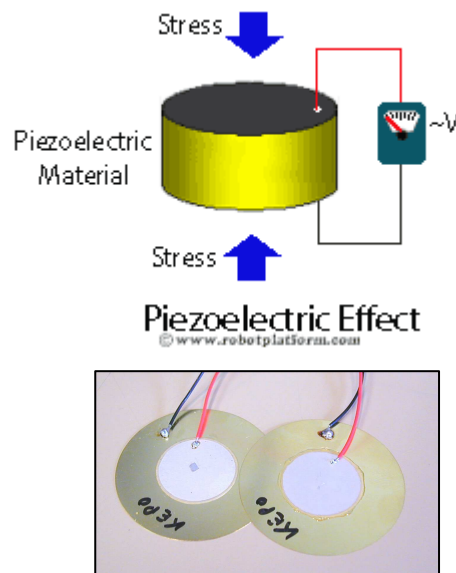
Different architectures

15

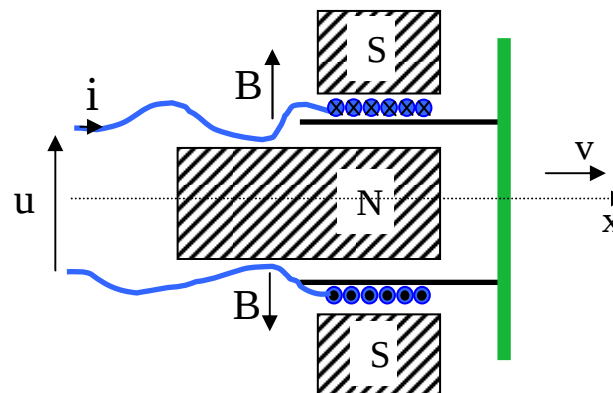


Electro-mechanical transducer

Piezoelectric sensors



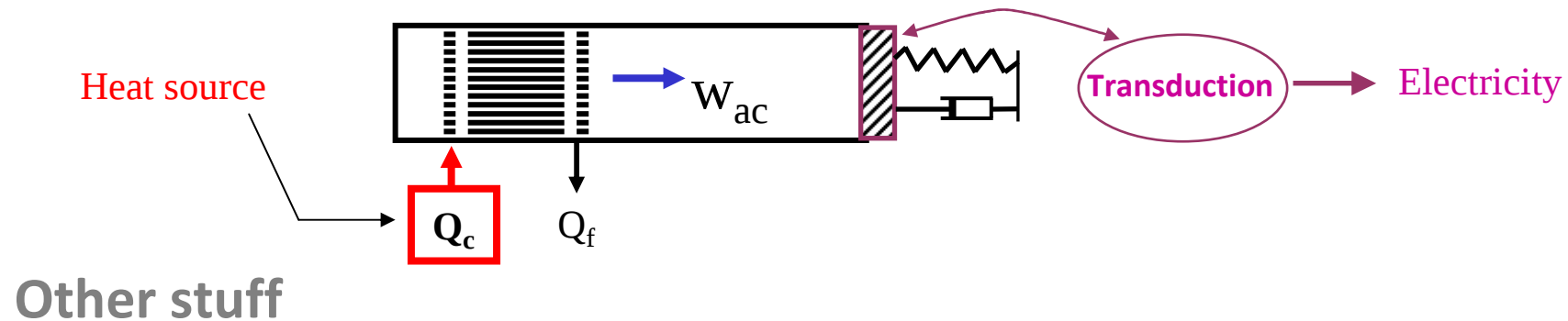
Electrodynamic sensors



Qdrive's 1S102M/A linear reciprocating motor/alternator

Different architectures

16



- ☐ Gaz
- ☐ Stack/regenerator material
- ☐ Heat exchangers
- ☐

Outlines

17

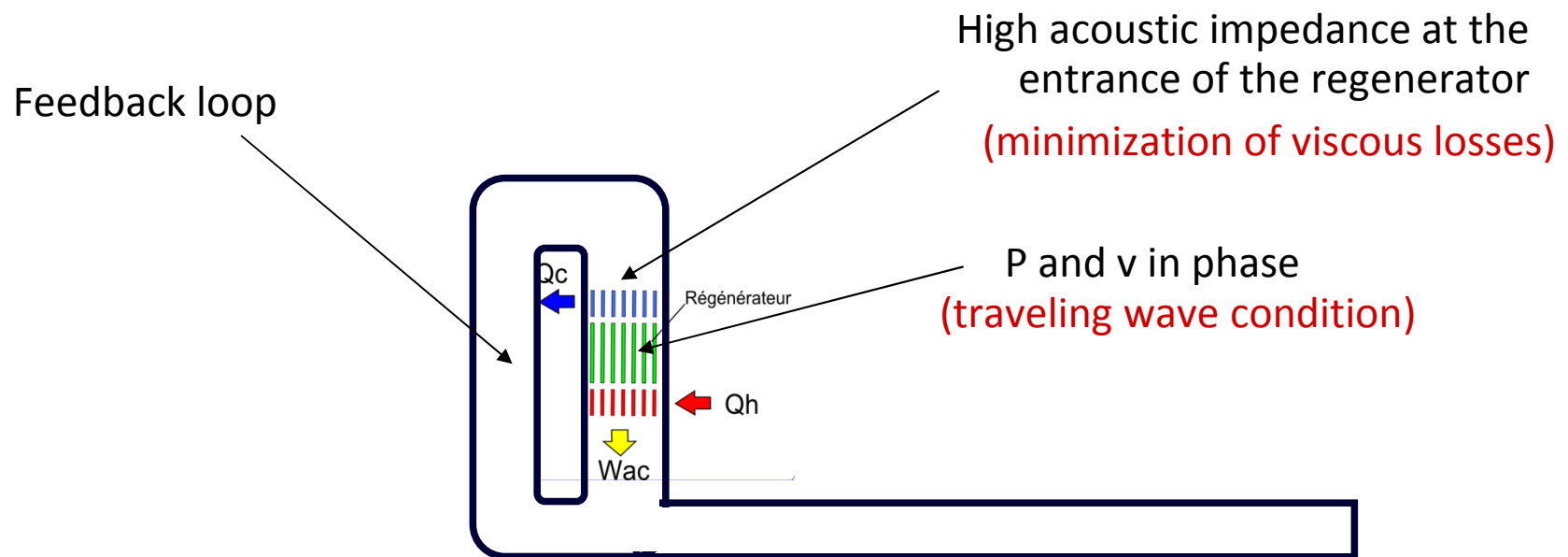
- Introduction
- **Theory**
- Some realizations
- Future development

Theory : engine design

18

- Case of traveling-wave loop thermoacoustic device

Analytical theory, but practically : **Use of Delta-EC** (or equivalent software)



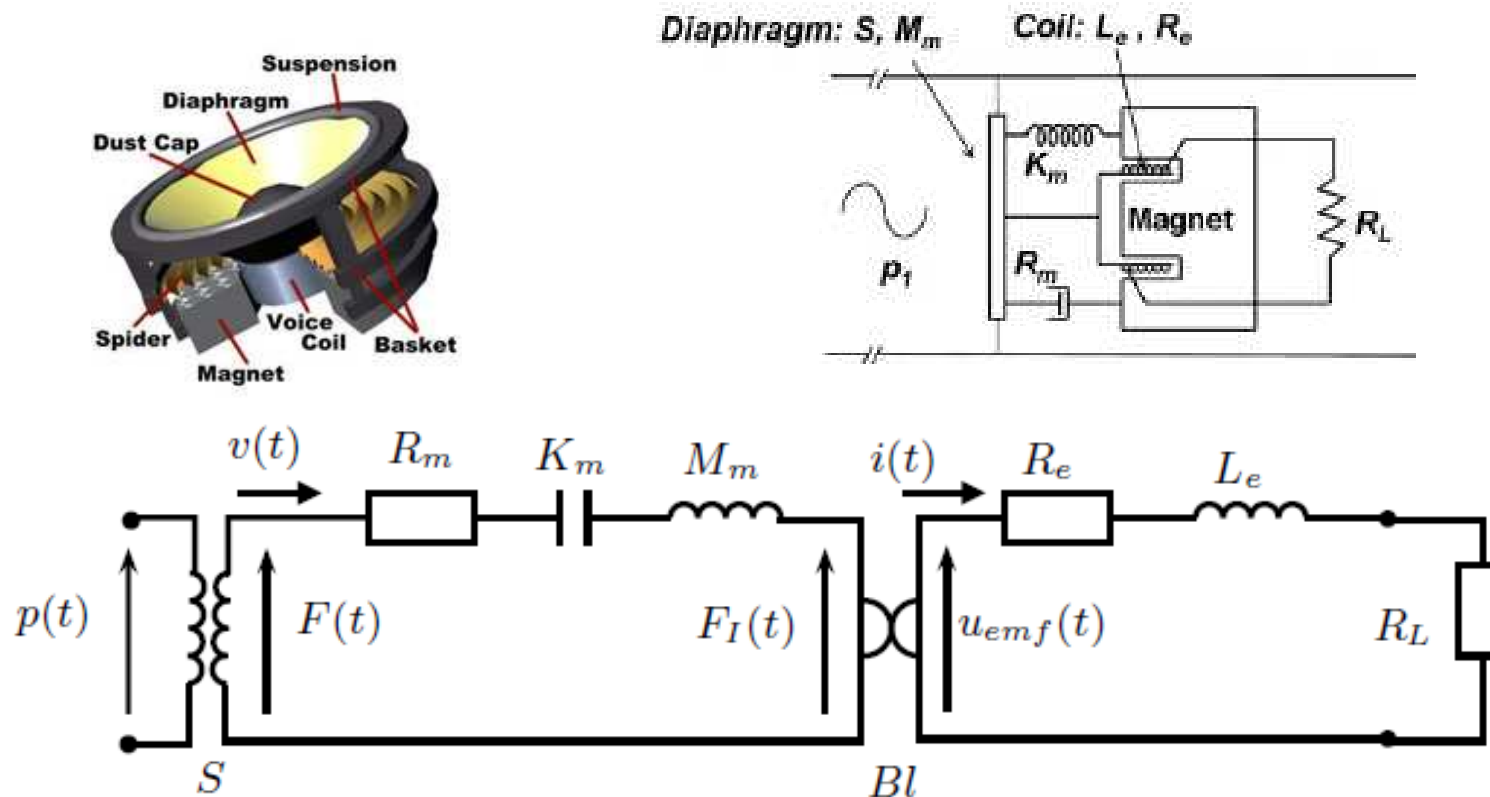
- Thermal to acoustic efficiency

$$\eta_{ta} = \frac{P_a}{Q_h}$$

Theory : acousto-electric coupling

19

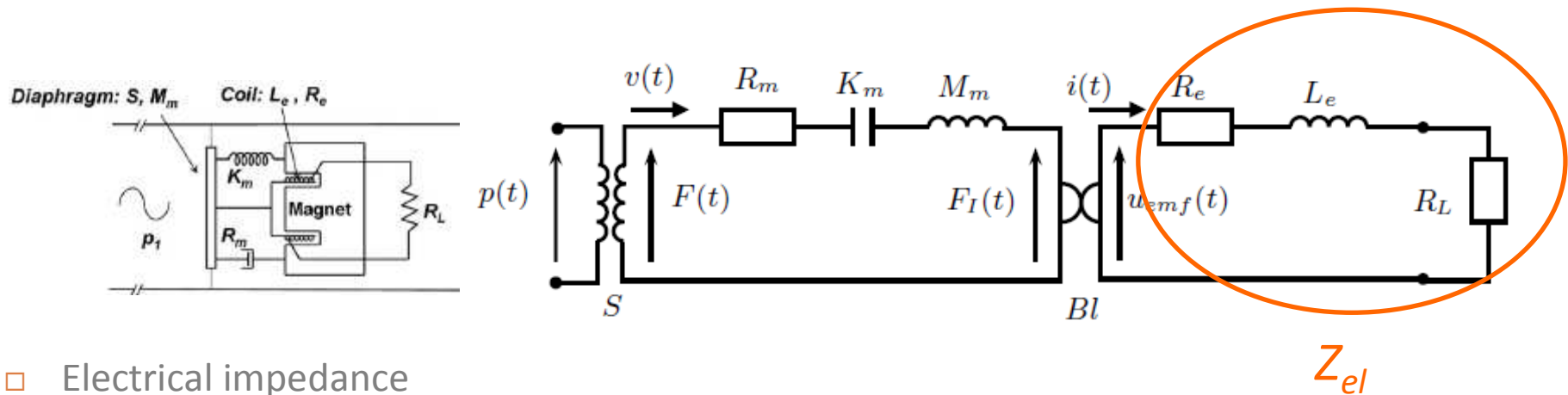
- Case of a linear alternator, seen as an electrodynamic loudspeaker



Electrical network equivalent to the alternator

Theory : acousto-electric coupling

20

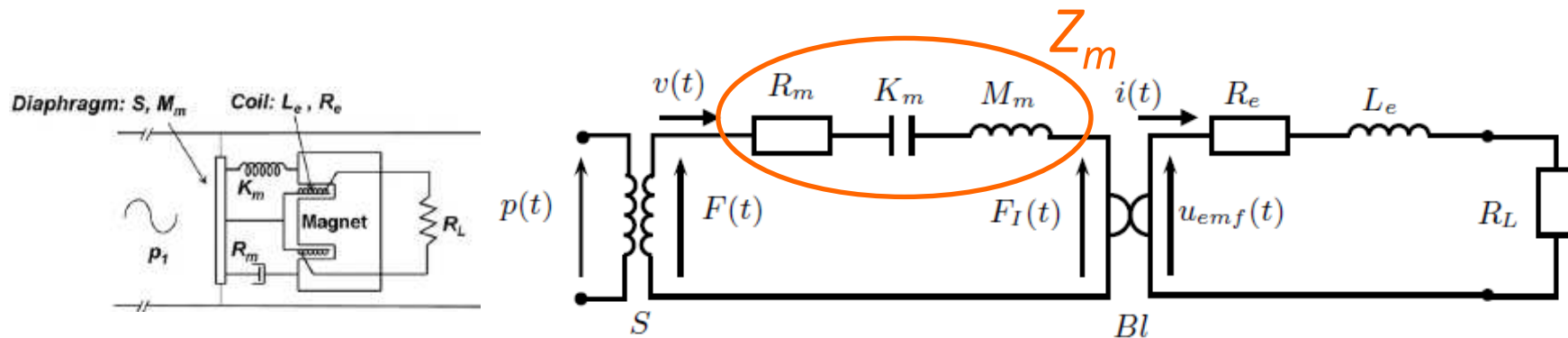


- Electrical impedance

$$Z_{el}(\omega) = R_e + j\omega L_e + R_L$$

Theory : acousto-electric coupling

21



- Electrical impedance

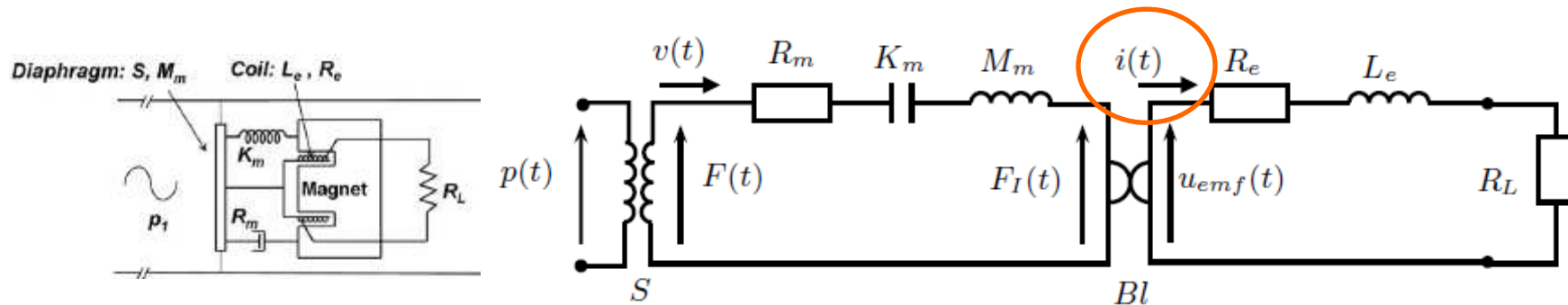
$$Z_{el}(\omega) = R_e + j\omega L_e + R_L$$

- Mechanical impedance

$$Z_m(\omega) = R_m + j\omega M_m - j\frac{K_m}{\omega}$$

Theory : acousto-electric coupling

22



- Electrical impedance

$$Z_{el}(\omega) = R_e + j\omega L_e + R_L$$

- Mechanical impedance

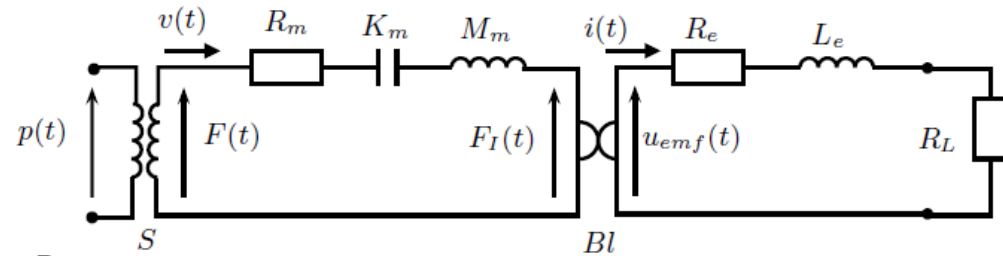
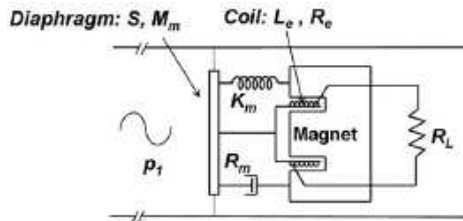
$$Z_m(\omega) = R_m + j\omega M_m - j\frac{K_m}{\omega}$$

- Electrical current flowing through the loading resistor R_L

$$I(\omega) = F(\omega) \left[\frac{Bl}{Z_e(\omega)Z_m(\omega) + Bl^2} \right] = p(\omega) \cdot S \left[\frac{Bl}{Z_e(\omega)Z_m(\omega) + Bl^2} \right]$$

Theory : acousto-electric coupling

23



- Electric power dissipated in resistor R_L

$$P_e(\omega) = \frac{1}{2} \Re\{I \cdot U^*\} = \frac{1}{2} |I(\omega)|^2 R_L = \frac{1}{2} |p(\omega)|^2 S^2 R_L \left| \frac{Bl}{Z_m(\omega) \cdot Z_{el}(\omega) + Bl^2} \right|^2$$

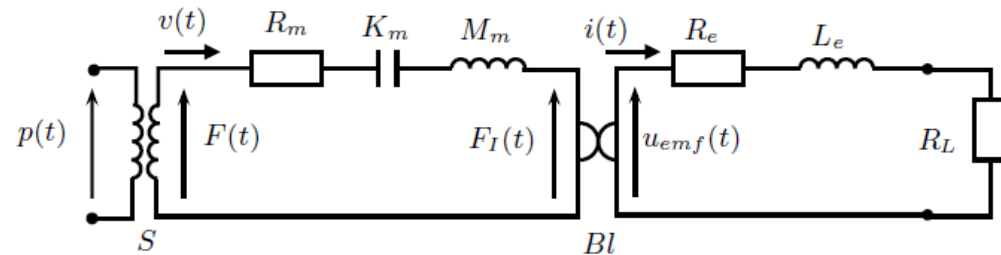
- Input acoustic power

$$P_a = \frac{1}{2} \Re\{p \cdot w^*\} = \frac{1}{2} \Re\left\{p \cdot \frac{p^*}{Z_a^*}\right\} = \frac{1}{2} |p|^2 \Re\left\{\frac{1}{Z_a}\right\} = \frac{1}{2} |p(\omega)|^2 S^2 \cdot \Re\left\{\frac{Z_{el}(\omega)}{Z_m(\omega) \cdot Z_{el}(\omega) + Bl^2}\right\}$$

$$\eta = \frac{P_e(\omega)}{P_a(\omega)} = \frac{R_L \left| \frac{Bl}{Z_m(\omega) \cdot Z_{el}(\omega) + Bl^2} \right|^2}{\Re\left\{\frac{Z_{el}(\omega)}{Z_m(\omega) \cdot Z_{el}(\omega) + Bl^2}\right\}}$$

Theory : acousto-electric coupling

24



- Acoustic to electrical efficiency

$$\eta = \frac{P_e(\omega)}{P_a(\omega)} = \frac{R_L \left| \frac{Bl}{Z_m(\omega) \cdot Z_{el}(\omega) + Bl^2} \right|^2}{\Re \left\{ \frac{Z_{el}(\omega)}{Z_m(\omega) \cdot Z_{el}(\omega) + Bl^2} \right\}}$$

- If $L_e \omega \ll R_e$, then $R_{el} \approx R_e + R_L$
- If $\omega = \omega_r$, then $Z_m = R_m$

$$\eta = \frac{Bl^2 R_L}{R_m \cdot (R_L + R_e)^2 + Bl^2 \cdot (R_L + R_e)}$$

Theory : thermo-electric coupling

25

□ Thermal to electrical efficiency $\eta_{te} = \frac{P_e}{Q_h}$

Not so easy to predict from separate study of each part of the device
Strong coupling between thermoacoustic resonator and alternator

The device has to be designed as a whole

Outlines

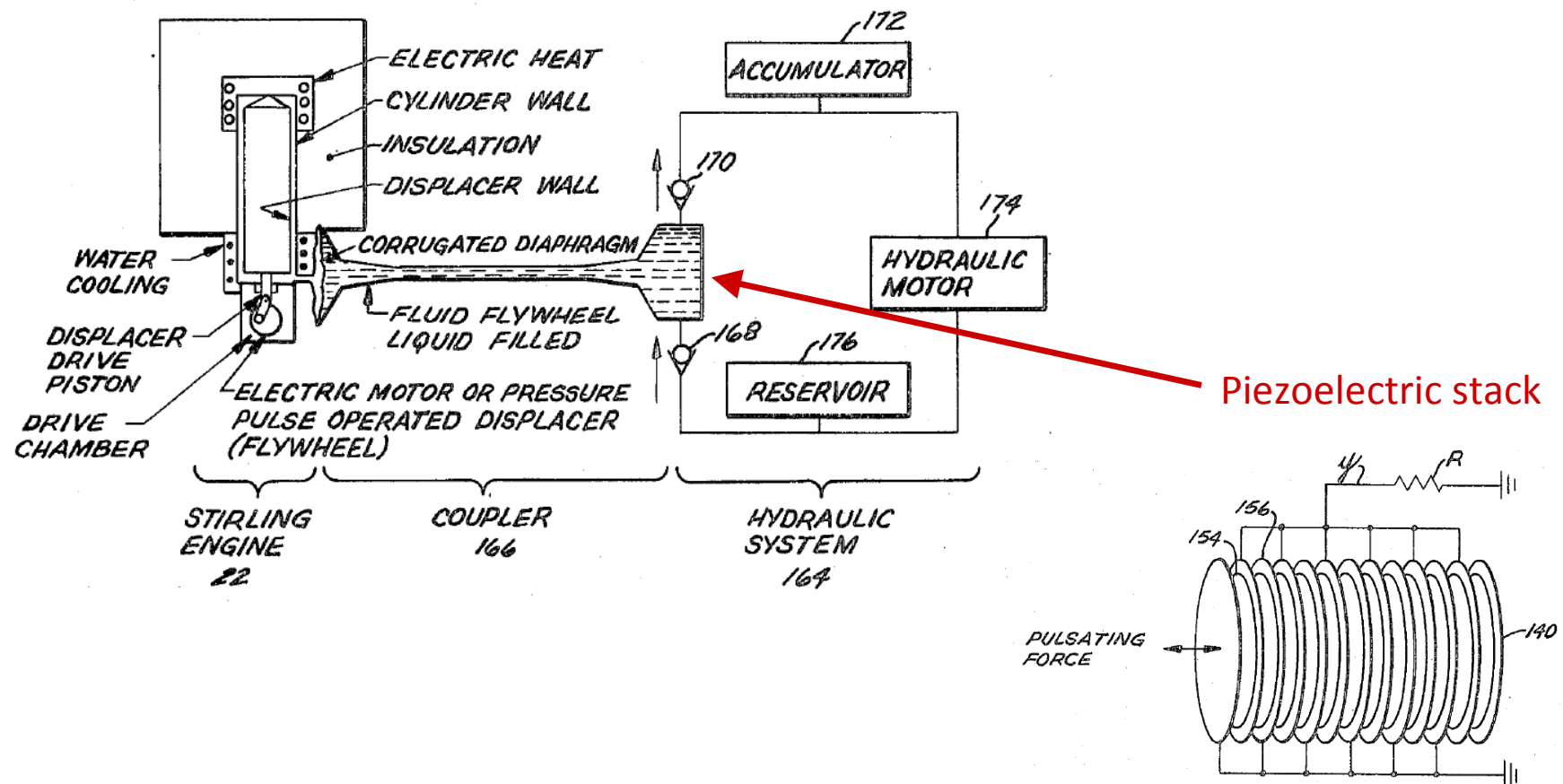
26

- Introduction
- Theory
- Some realizations (**non-exhaustive**)
- Future development

Standing waves devices

27

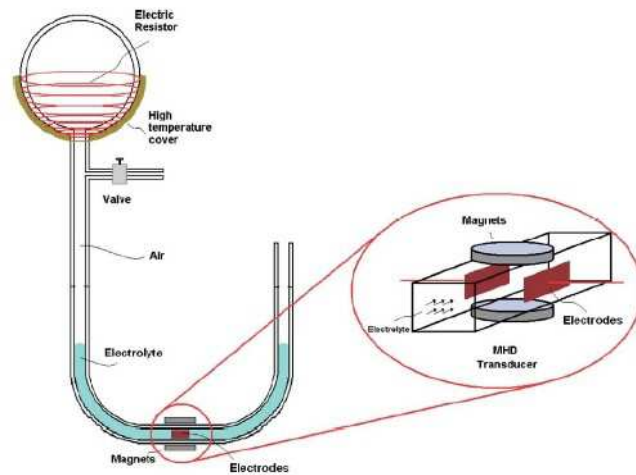
Martini et al. , Stirling engine power system, US Patent (1974)



Standing waves devices

28

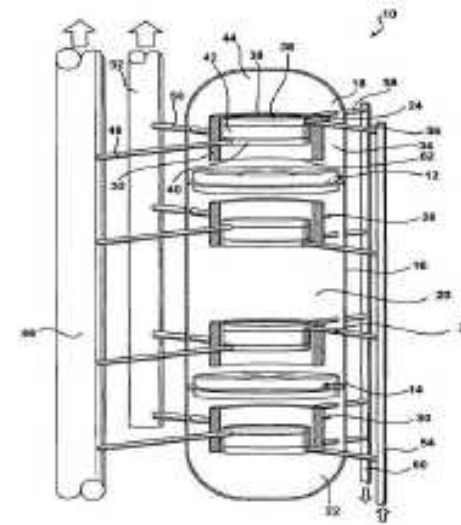
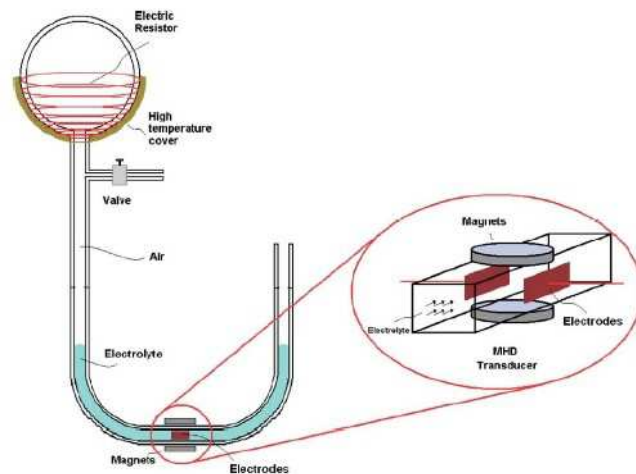
Huelsz et al., Magneto-hydro-dynamical transduction, 2006



Standing waves devices

29

Huelsz et al., Magneto-hydro-dynamical transduction, 2006



Keolian et al. , Thermoacoustic piezoelectric generator,
US Patent (2010)

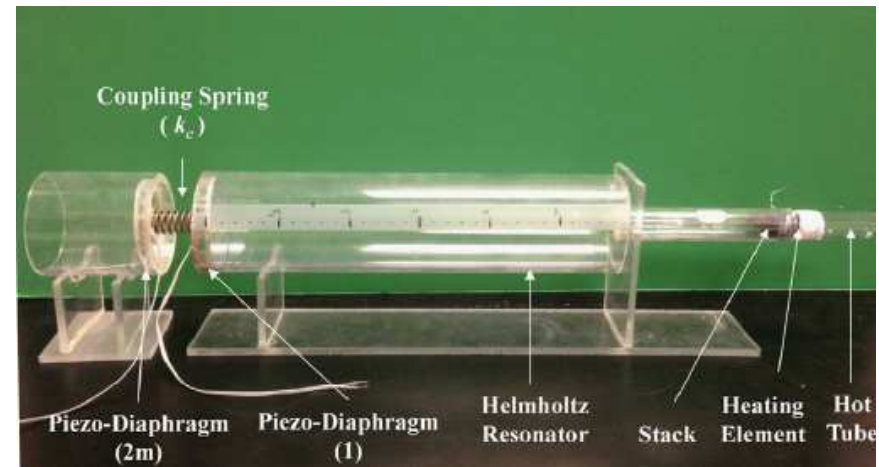
Application : Diesel truck waste heat recovery

Standing waves devices

30

Last development in Energy harvesting
Smoker et al., Nouh et al., 2012 - 2014

- Input heating power : $Q_h = 40 \text{ W}$
- Output electric power : $P_{el} = 0,12 \text{ mW}$
- Acoustic to electric efficiency : $\eta_{ae} \approx 10\%$
- Global efficiency : $\eta \approx 3 \cdot 10^{-4}\%$



Low efficiency, but can be miniaturized and distributed

□ Still in progress...

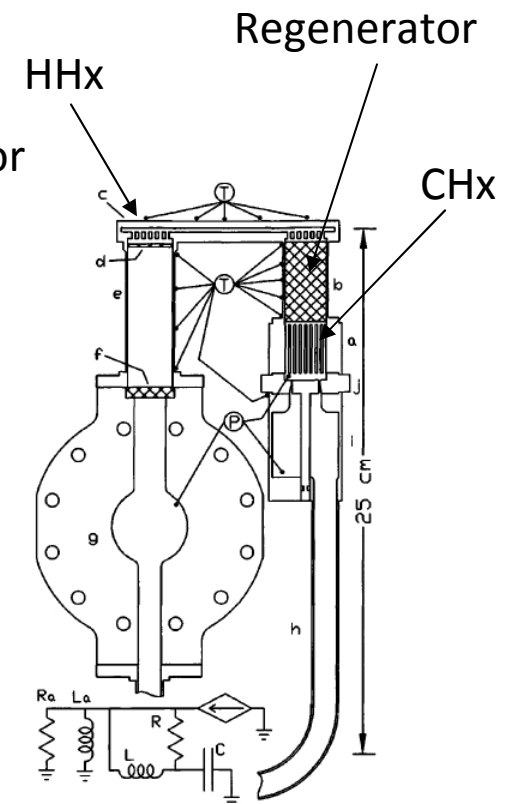
Traveling waves devices

31

S. Backhaus et al., Los Alamos Lab., 2004



Electrodynamic alternator



- Fluide : He, 55 Bar
- Volume :
 $V_{cavarr} = 0.6 \text{ l}$,
 $V_{tot} > 2 \text{ l}$
- Performance :
 $f \approx 120 \text{ Hz}$
 $T_h \approx 600 \text{ }^\circ\text{C}$
 $Q_h < 400 \text{ W}$
 $Q_{el_{max}} \approx 58 \text{ W}$
 $\eta_{max} \approx 18 \%$

Traveling waves devices

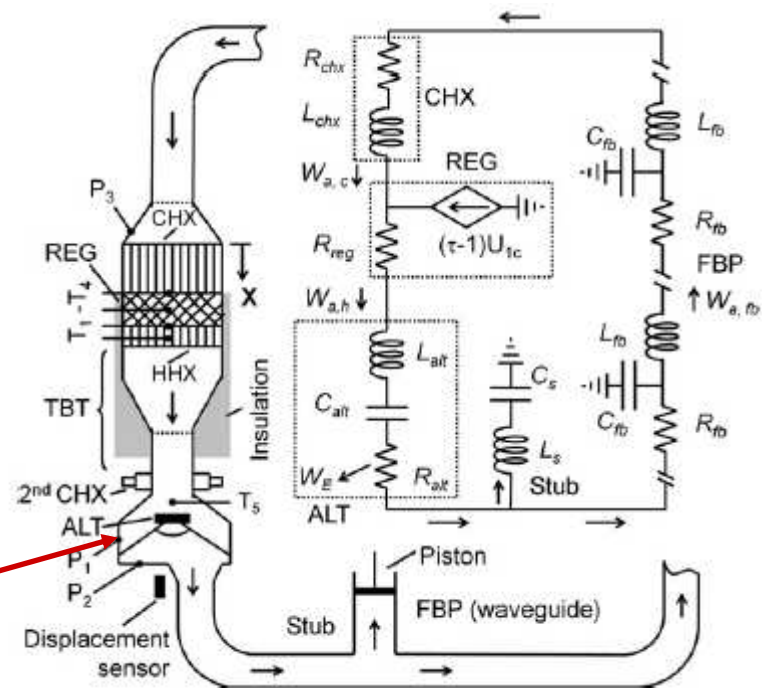
32

Yu et al., Score project, 2012

Low cost electricity generator for rural area driven by biomass

- **Fluide** : air, 1 Bar
- **Volume** :
 $L \approx 4.25 \text{ m}$, $R = 2.7 \text{ à } 6.4 \text{ cm}$
 $V_{tot} > 10 \text{ l}$
- **Performance** :
 $f \approx 70 \text{ Hz}$
 $T_h \approx 120 \text{ °C}$
 $Q_h < 500 \text{ W}$
 $Q_{elmax} \approx 11.6 \text{ W}$
 $\eta_{max} \approx 3 \%$

Classical loudspeaker set in the loop



Traveling waves devices

33

Hekyom, 2011 : Demonstrator of thermoacoustic electricity generator

□ $P_{el} = 800 \text{ W}$

□ $T_h = 950 \text{ }^{\circ}\text{C}$

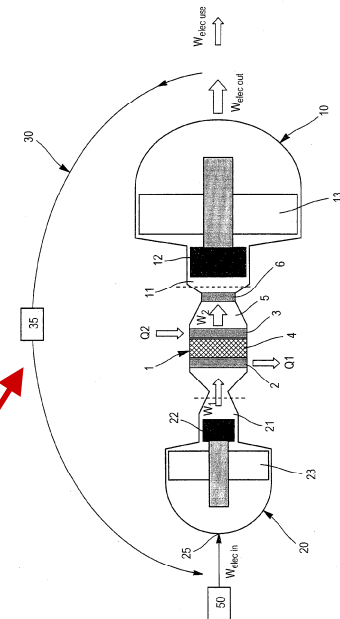
2 Q-Drive transducers



WO 2011/098735

PCT/FR2011/050284

2/9



Electric feedback loop

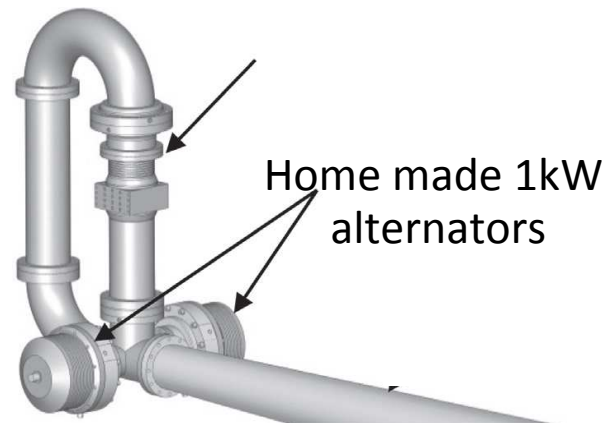
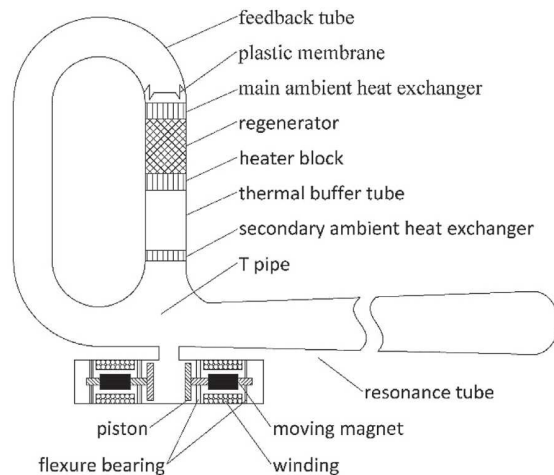
□ For more information, ask M. X. FRANCOIS

Traveling waves devices

34

Research Program of China, 2010 – 2014, Sun et al., Wu et al.

Thermoacoustic electric generator coupled to a solar dish



□ **Fluide :** He (95,5%) Ar (4,5%), 40 Bar

□ **Performance :**

$$f = 64 \text{ Hz}$$

$$T_h = 650 \text{ }^{\circ}\text{C}$$

$$P_{el \text{ max}} \approx 1040 \text{ W (*)}$$

$$\eta_{\text{max}} \approx 19,8\% (*)$$

** In lab conditions*

Traveling waves devices

35

Qnergy, TASE-3 project, 2014

Produces 1 kW of electrical power during solar operation



Qnergy's TASE-3 thermoacoustic Stirling engine during operation at the company's test facility in Ogden, Utah.

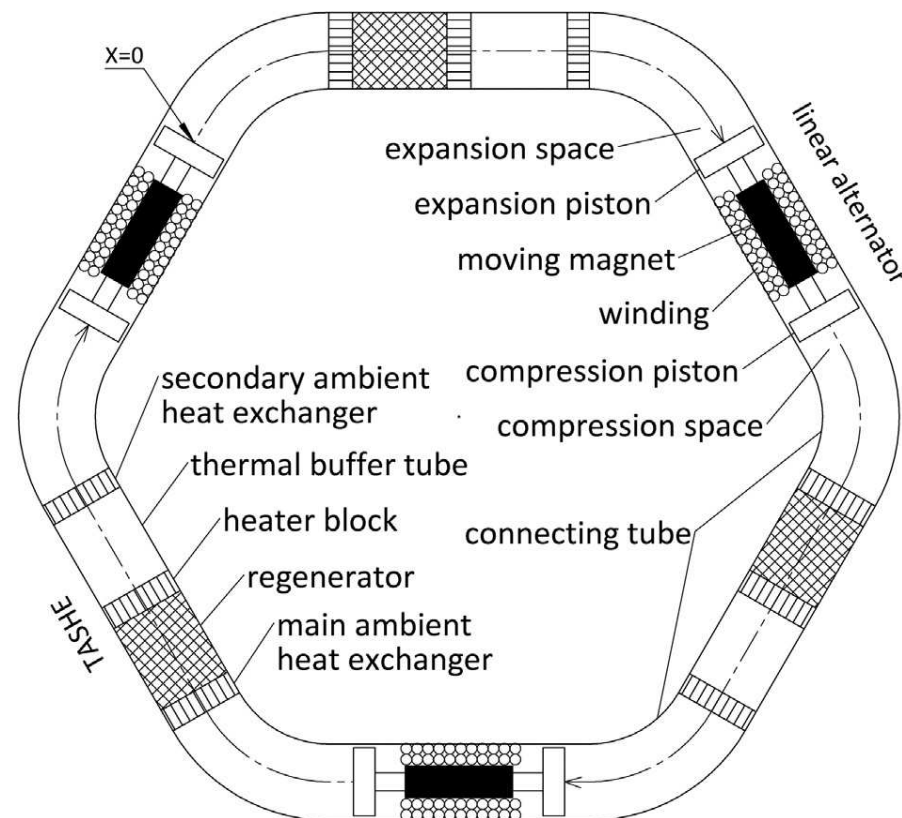
Traveling waves devices

36

Research Program of China, 2014, Wu et al.

3 kW double-acting thermoacoustic Stirling electric generator

- Fluide : He 50 Bar
- Performance :
 - $f = 86 \text{ Hz}$
 - $T_h = 650 \text{ }^\circ\text{C}$
 - $P_{el \text{ max}} \approx 1570 \text{ W}$
 - $\eta_{\text{max}} \approx 16,8\%$



Outlines

37

- Introduction
- Theory
- Some realizations
- **Future development**

Future development

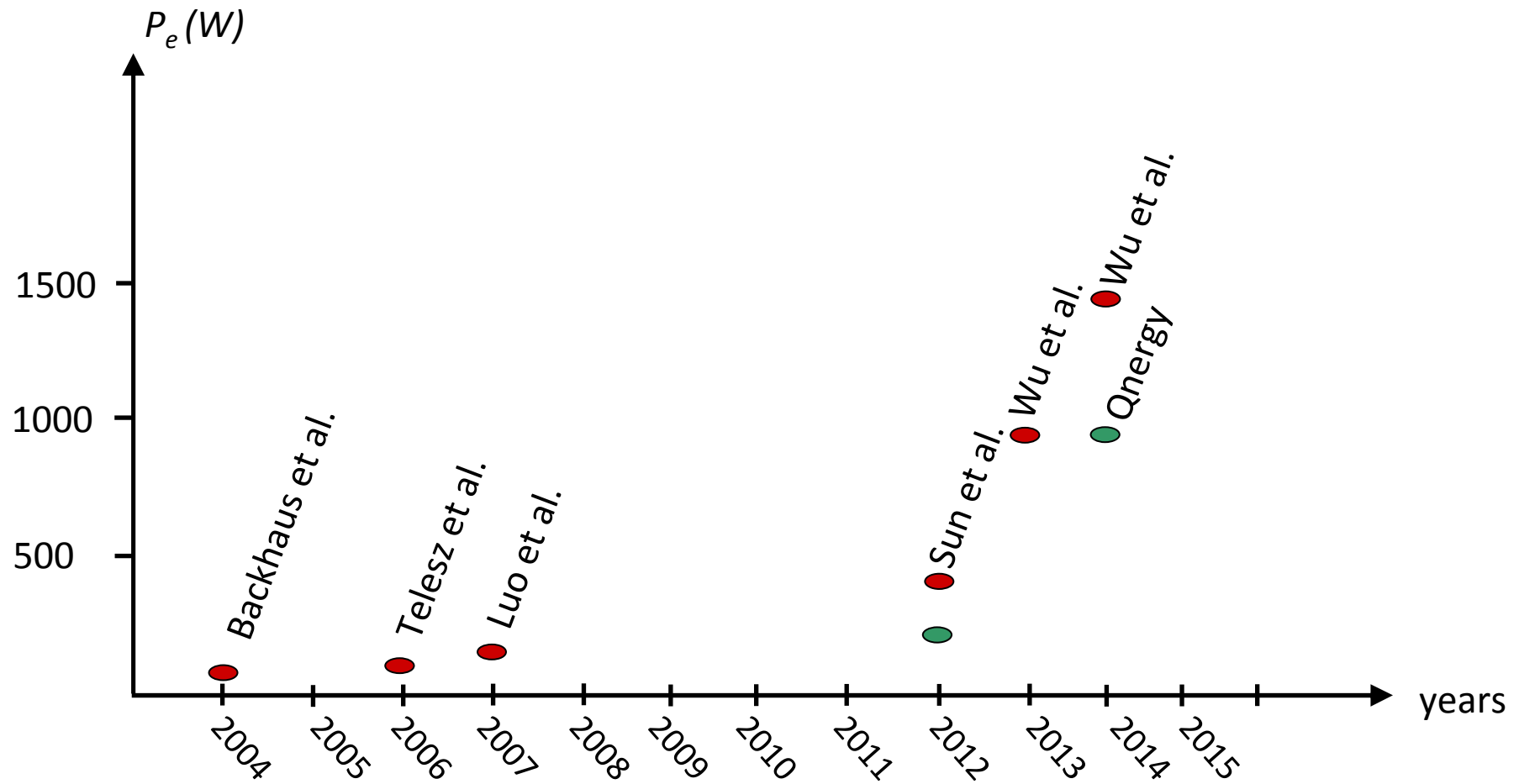
38

Key points

- Heat exchangers
- Alternators
- Thermoacoustic process

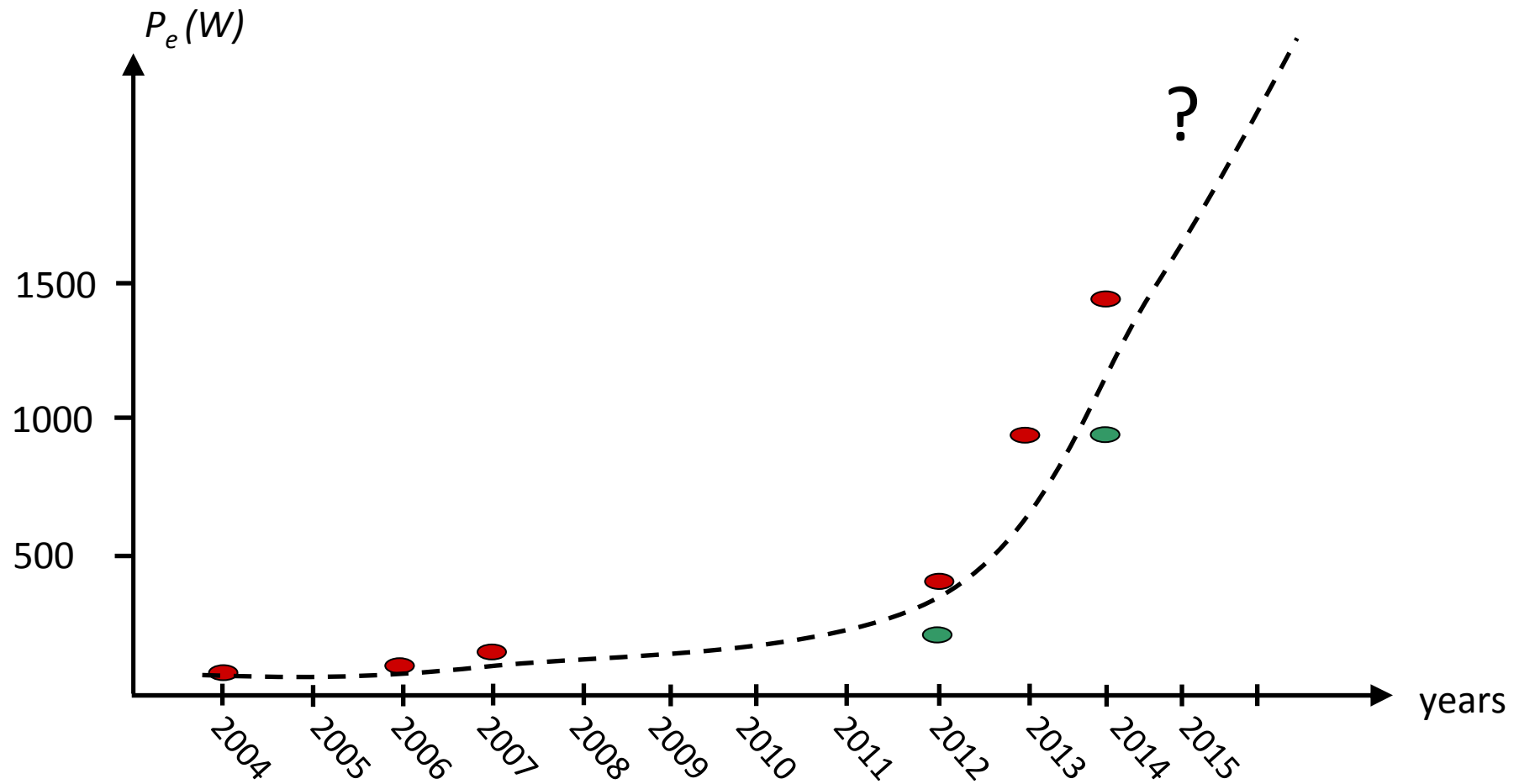
Future development

39



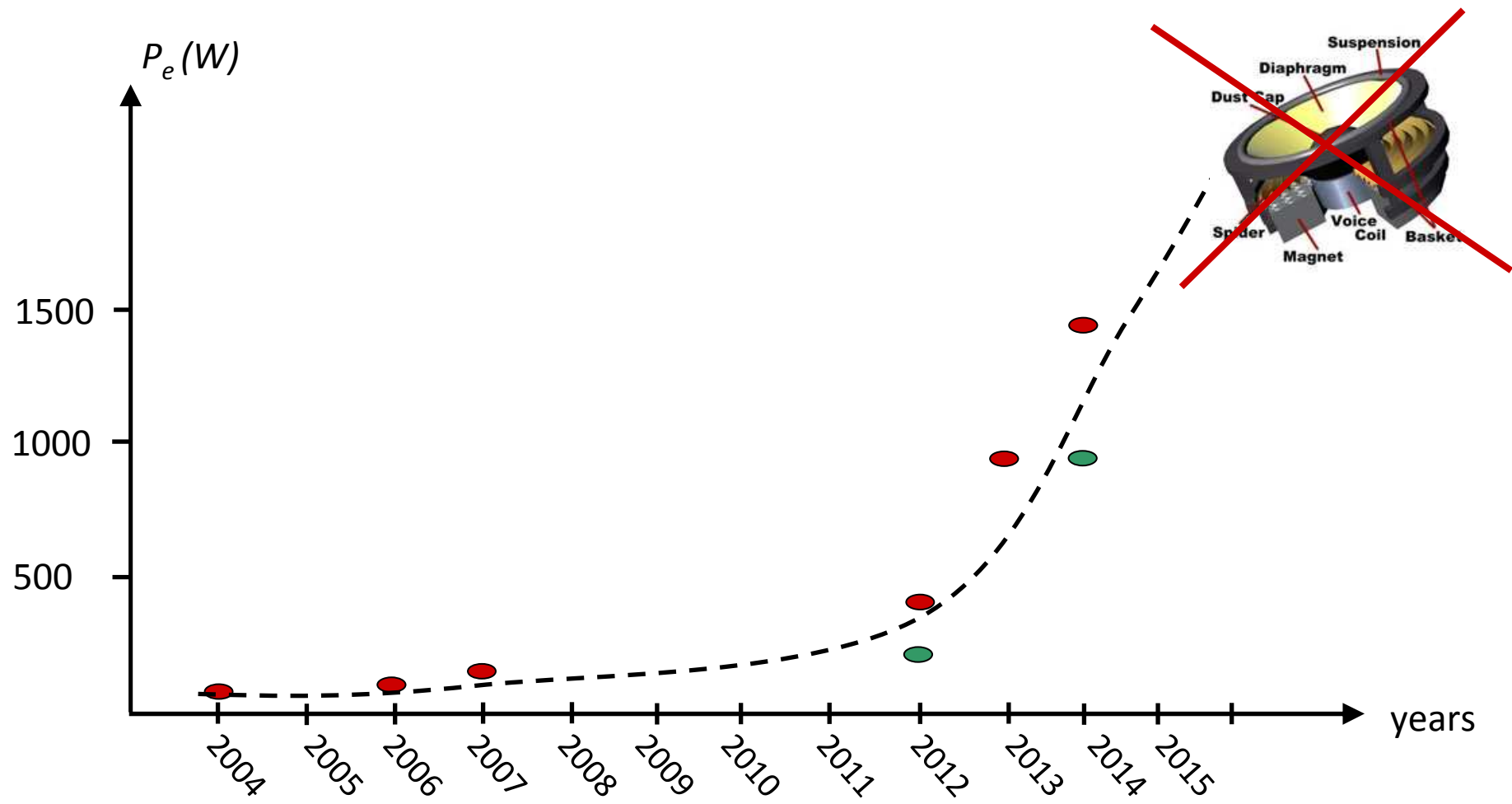
Future development

40



Future development

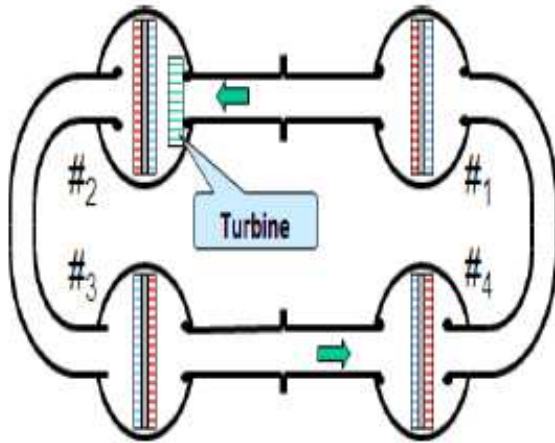
41



Other alternators?

42

Thermo Acoustic Power Program, ASTER, K. de Block, 2013

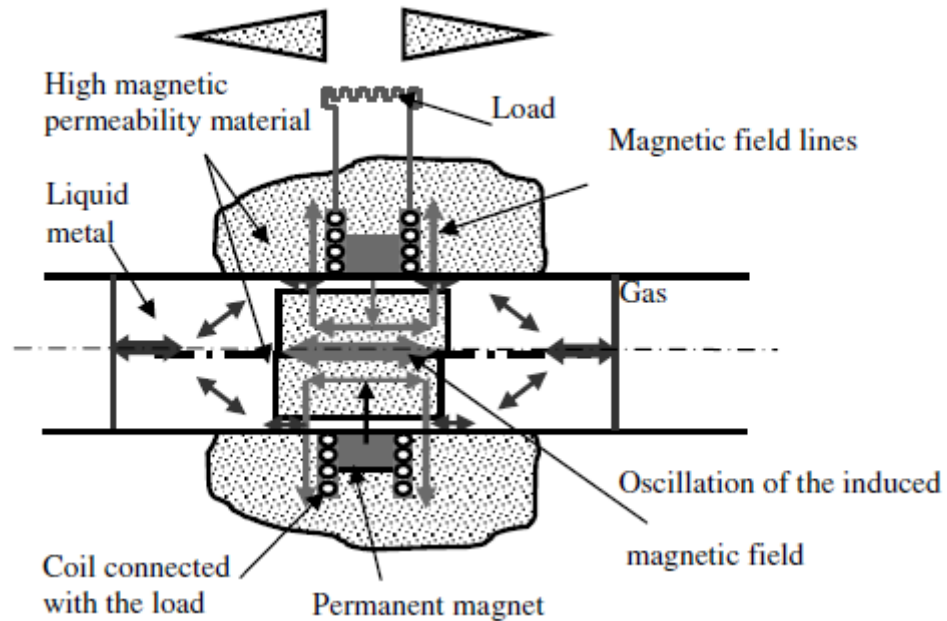


□ For more information, ask K. de Block

Other alternators?

43

MHD Electric Generator, A. Alemany et al., 2010



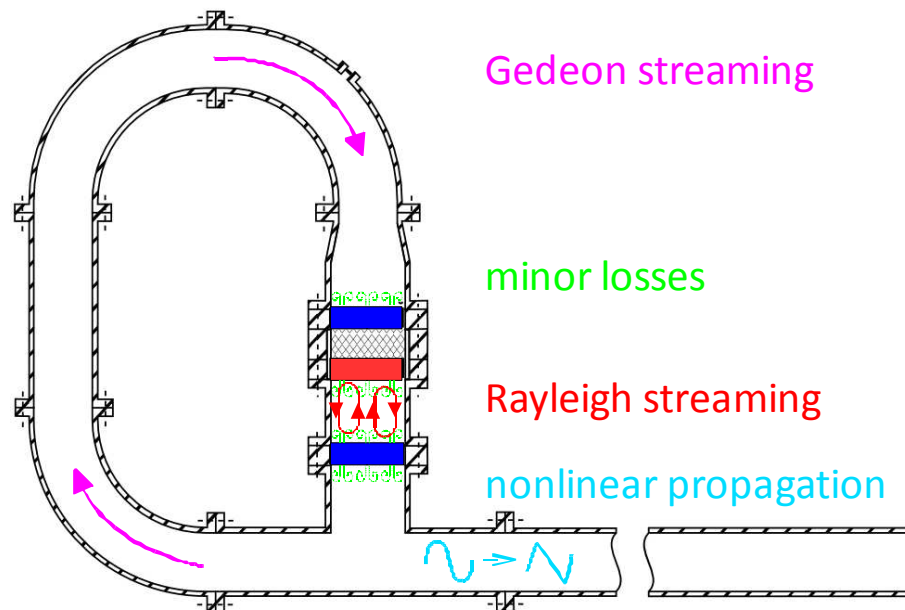
- For more information, see presentation of A. Alemany

Thermoacoustic process optimization

44

□ Control of non linear effects

- For example : Acoustic streaming



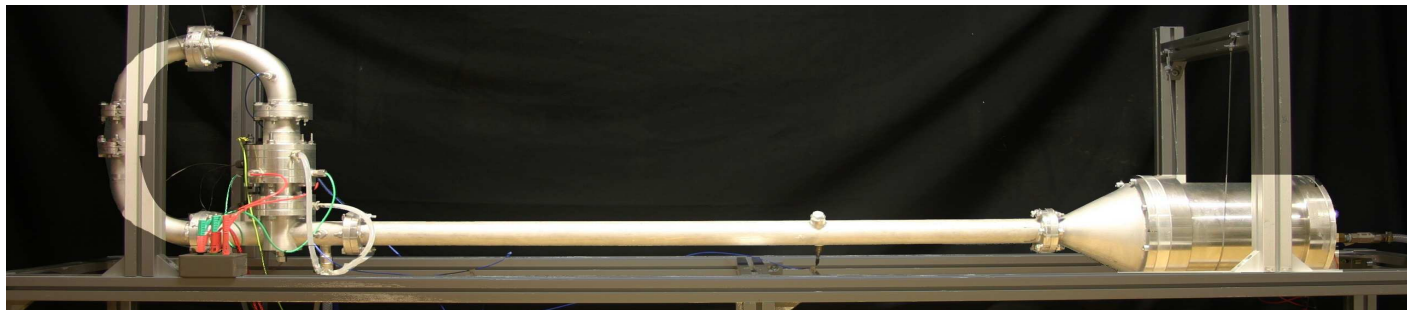
- For more information, see presentation of H. Bailliet

Thermoacoustic process optimization

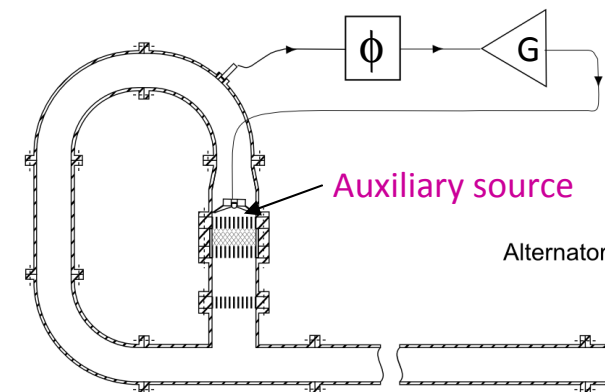
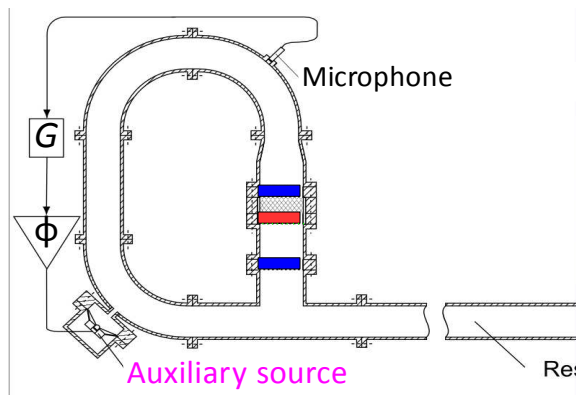
45

- Active tuning of acoustic oscillations in a thermo-acoustic power generator

Work in progress at « Laboratoire d'Acoustique de l'Université du Maine » (LAUM)



Experimental setup

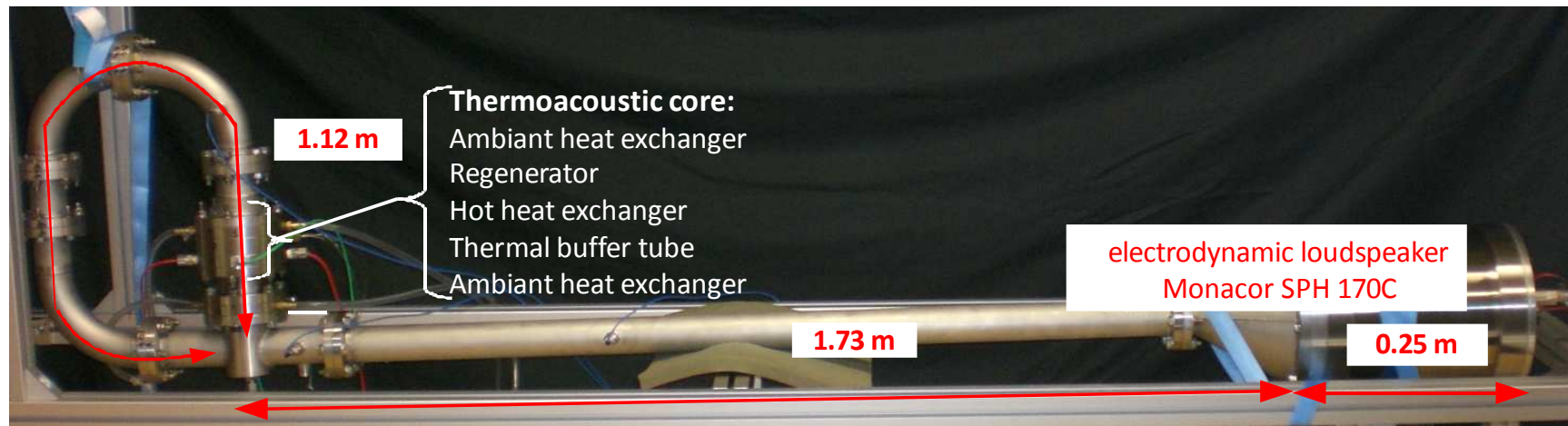


[1] C. Olivier, G. Penelet, G. Poignand and P. Lotton . « Active control of thermoacoustic amplification in a thermo-acousto-electric engine », *Journal of Applied Physics*, vol. 115 [17], 2014.

Thermoacoustic process optimization

46

- Active tuning of acoustic oscillations in a thermo-acoustic power generator



- Fluid : air
- Static pressure : 5 Bars
- Ambient temperature : 295 K

- Frequency: 40 Hz
- Onset condition: $Q_h = 60 \text{ W}, \Delta T = 401 \text{ K}$
- Above onset: $Q_h = 70 \text{ W}, \text{DR} = 1 \%, \eta_\phi = 0.24 \%, \Delta T_\phi = 407.7 \text{ K}$
 $Q_h = 140 \text{ W}, \text{DR} = 3.2 \%, \eta_\phi = 0.71 \%, \Delta T_\phi = 452 \text{ K}$
- Low efficiency: engine = study model (modular, limited budget, low efficiency alternator) but designed to work closed to its maximum value.

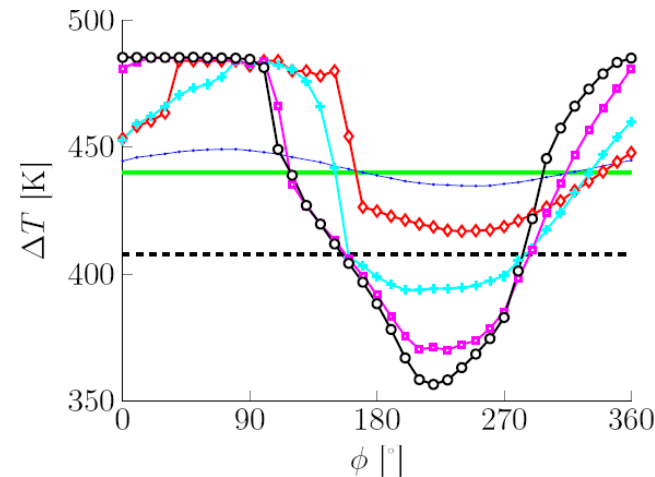
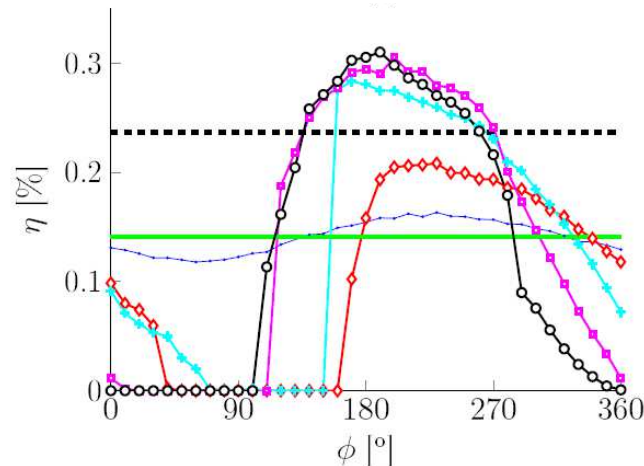
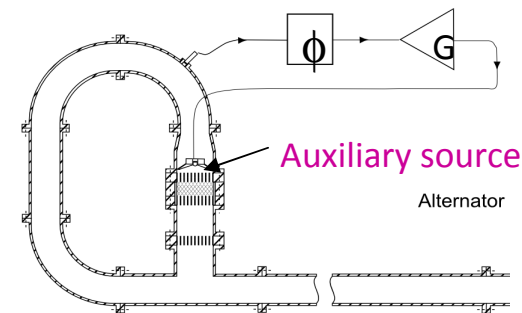
Thermoacoustic process optimization

47

- Experimental results : case with internal auxiliary source

$$\eta = \frac{W_{el}(G=0) + \Delta W_{el}}{Q_h + W_{Is}}$$

- Efficiency η versus ϕ for different G

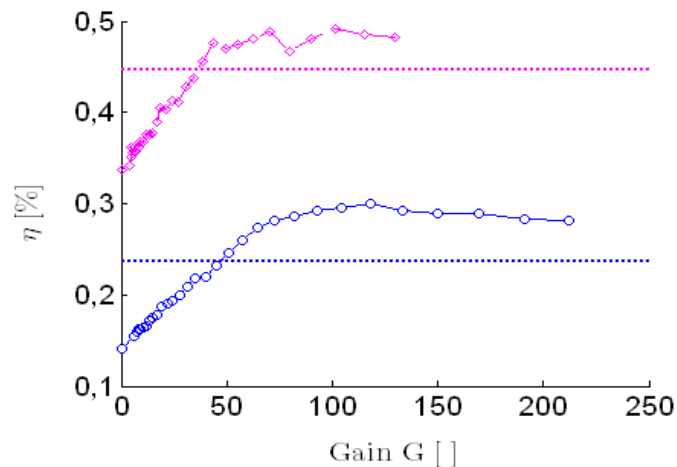


$Q_h = 70 \text{ W}$, $G = 0$ (-), 10 (-), 40 ($\diamond$), 70 (+), 135 ($\square$) or 190(o),
without active control (--)

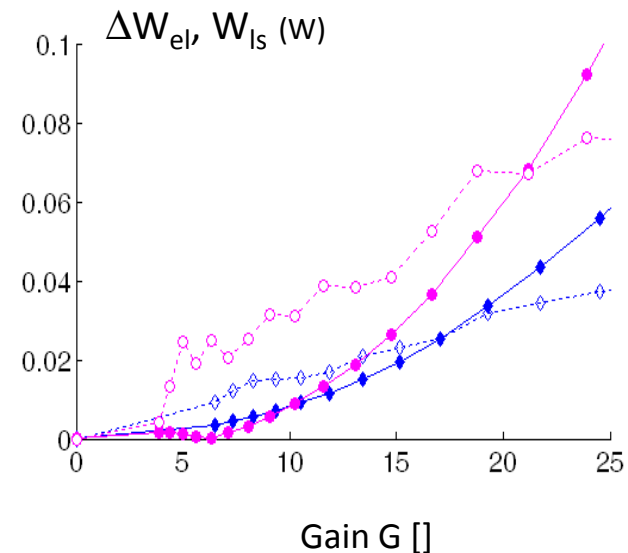
Thermoacoustic process optimization

48

- Efficiency η versus G for $\phi = \phi$ optimal



$Q_h = 70$ W (○), 100W (○), without active control (..)



- ΔW_{el} (○) : additional power produced
- W_{ls} (●) : power supplied to the auxiliary source

Thermoacoustic process optimization

49

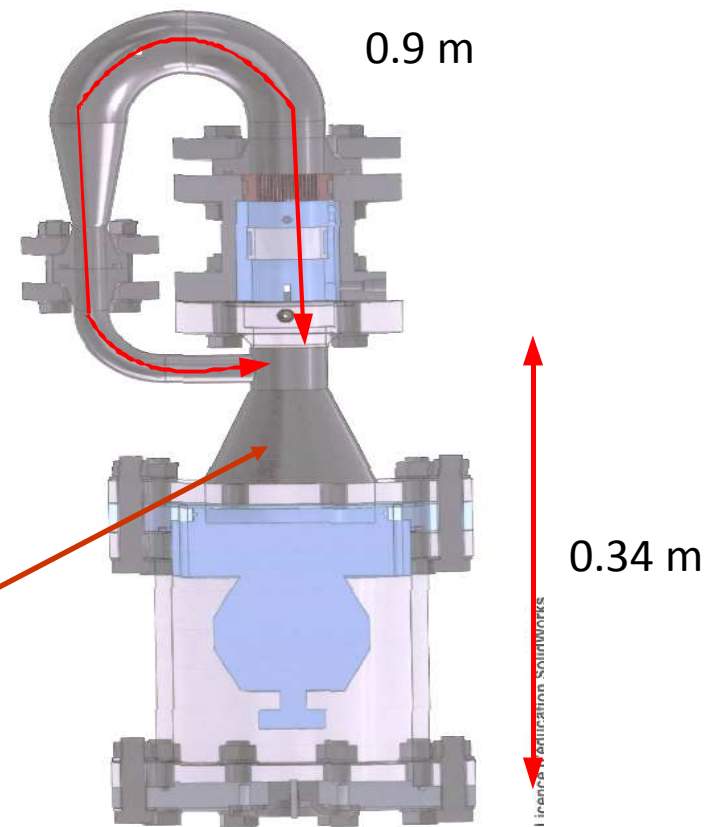
- Active control applied on a high power thermoacoustic compact engine (currently being built at LAUM)

- Fluid : **helium**
- Static pressure : **22 Bars**

- Heat input : **1000 W**
- Efficiency (theoretical): **20 %**
- Electric power: **200 W**

alternator:
Qdrive 1S 132D

Work in progress ...





Thank you for your attention . . .

The thermoacoustic team



Pierrick LOTTON
(Senior Researcher)



Guillaume PENELET
(Associate Professor)



Gaëlle POIGNAND
(Research Engineer)



Côme OLIVIER
(PhD Student)